cont A1 degraded.

Page 3, please replace the paragraph numbered [0014] as follows:

A2 When the core diameter is smaller than 0.38D, the flexural rigidity of the tool will be insufficient, and when the core diameter is larger than 0.42D, the space inside the chip discharging grooves will be too small so that the chips will accumulate therein.

Page 5, please replace the paragraph numbered [0031] as follows:

A3 Figs. 6a-6f are schematic representations showing the results of a second test, in which examples of the present invention and comparative examples were compated.

Page 7, please replace the paragraph numbered [0042] as follows:

A4 As shown in FIG. 1 and FIG. 3, the land portions 10 and 10 are separated by the pair of chip discharging grooves 6, 6. A diameter of a core 14 in the middle of the land portions 10 and 10 is in the range of 0.38D to 0.42D, in which D is the cutting edge diameter representing the distance between the peripheral ends of the cutting edges 8, 8. When the core diameter is smaller than 0.38D, the flexural rigidity of the main body 2 will be reduced. When the core diameter is larger than 0.42D, the depth of the chip discharging grooves 6, 6 will be small and the space therein will be insufficient, so that the chips will clump inside the chip discharging grooves 6, 6, increasing the cutting force. As a result, fracture and wearing of the cutting edges 8 and 8 will occur. Accordingly, there will be problems in that the cutting accuracy will be degraded and the tool life will be reduced in either case.

Page 12, please replace the paragraph numbered [0063] as follows:

A5 With respect to each of types A and D, three samples were used in this test. The results of the test are shown in Figs. 6a-6f.

Page 12, please replace the paragraph numbered [0064] as follows:

A6 First, holes were formed under conditions in which the feed was fixed to 0.10 mm/rev

Cont A6 and the cutting speed was icnreased from 1 to 20 m/min, and the amounts of oversizing in the formed holes were measured (see Fig. 6a). Next, holes were formed under conditions in which the cutting speed was fixed to 20 m/min, the feed was increased to 0.10 mm/rev, and the amounts of oversizing in the formed holes were measured (see Fig. 6d).

Page 12, please replace the paragraph numbered [0065] as follows:

A7 The degree of variation in the amounts of oversizing in the holes formed by the samples of type D was larger compared to the holes formed by the samples of type A. In the case in which the feed was fixed, the sample of type D broke when the cutting speed was 20 m/min, as is understood from Figs. 6a-6d. In the case in which the cutting speed was fixed, the sample of type D broke when the fee was 0.10 mm/rev, as is understood from Figs 6c-6f.

Page 12 and 13, please replace the paragraph numbered [0066] as follows:

A8 First, holes were formed under conditions in which the feed was fixed to 0.10 mm/rev and the cutting speed was increased from 1 to 20 m/min, and surface roughnesses of the formed holes were measured (see Fig.6b). Next, holes were formed under conditions in which the cutting speed was fixed to 20 m/min, the feed was increased to 0.10 mm/rev, and the surface roughnesses of the formed holes were measured (see Fig. 6e).

Page 13, please replace the paragraph numbered [0067] as follows:

A9 The degree of variation in the surface roughnesses of the holes formed by the samples of type D was larger compared to the holes formed by the samples of type A. In the case in which the feed was fixed, the sample of type D broke when the cutting speed was 20 m/min, as is understood from Figs. 6a-6c. In the case in which the cutting speed was fixed, the sample of type D broke when the feed was 0.10 mm/rev, as is understood from Figs. 6d-6f.

Page 13, please replace the paragraph numbered [0068] as follows:

A10 First, holes were formed under conditions in which the feed was fixed to 0.10 mm/rev

Cont A10 and the cutting speed was increased from 1 to 24 m/min, and the circularity of each of the formed holes were measured (see Fig. 6c). Next, holes were formed under conditions in which the cutting speed was fixed to 20 m/min and the feed was increased to 0.10 mm/rev, and the circularities of the formed holes were measured (see Fig. 6f).

Page 13, please replace the paragraph number [0069] as follows:

The circularities of the holes formed by the samples of type D were larger compared to the holes formed by the samples of type A. In the case in which the feed was fixed, the sample of type D broke when the cutting speed was 20 m/min, as is understood from Figs. 6a-6c. In the case in which the cutting speed was fixed, the sample of type D broke when the feed was 0.10 mm/rev, as is understood from Figs. 6d-6f. In, a third test, the variation in the amounts of abrasion in the flank face and the variation in the amounts of oversizing were examined.

A11

Please delete page 16 in its entirety.

IN THE CLAIMS

Please amend Claims 1, 3-8, 10-12, and 14-17 as follows:

1. (Amended) A hole forming tool which rotates around a rotational axis, comprising:

one or more chip discharging grooves which are helically formed around a rotational axis in an exterior surface of said hole forming tool, said chip discharging grooves having an inner surface; and

A12

one or more cutting edges which are formed along ridge lines between inner surfaces of said chip discharging grooves, which are facing the rotating direction, and flank faces formed at an end of said hole forming tool,